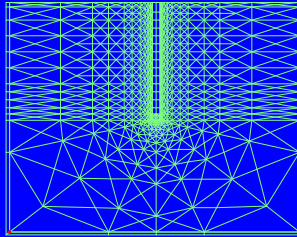


End bearing pile problem in granular material

16th CUGM at South Bank University



by Yong-Joo LEE

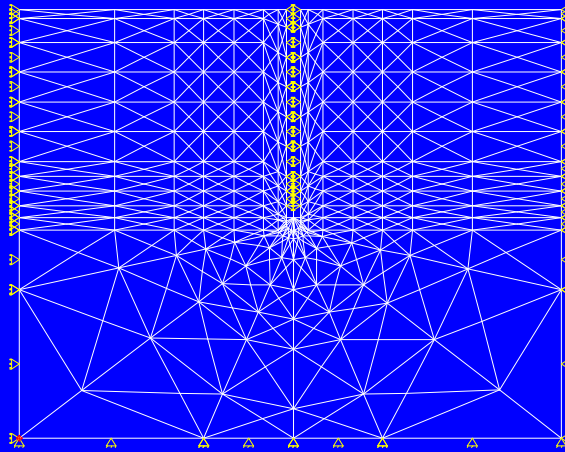
Soil Mechanics Group,

Civil and Environmental Engineering Department,
University College London

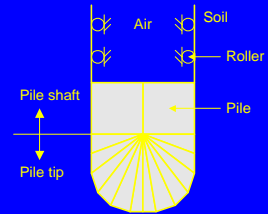
Objectives of this study:

- Comparison between **roller boundary** and **slip elements** for an end bearing pile in the granular material;
- Investigation of **degree of non-associated flow** in relation to the numerical convergence under D-MNR;
- Investigation of **boundary conditions**;
- Insight into **strain behaviour** at large pile displacement.

Mesh-A* (roller boundary along pile shaft)

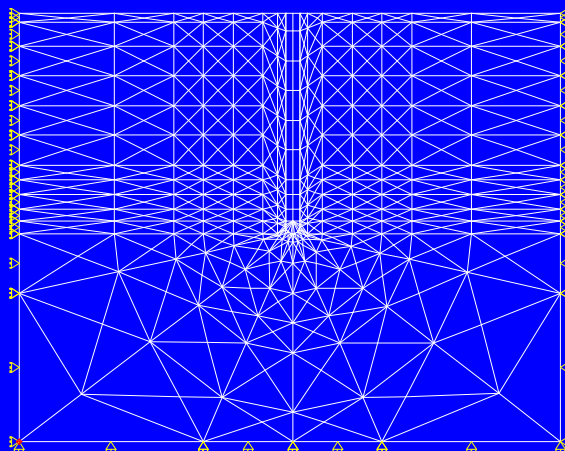


(464 nodes and 872 elements)

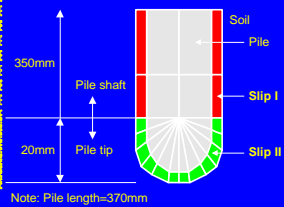


Pure end
bearing pile

Mesh-A (slip element types, I and II)

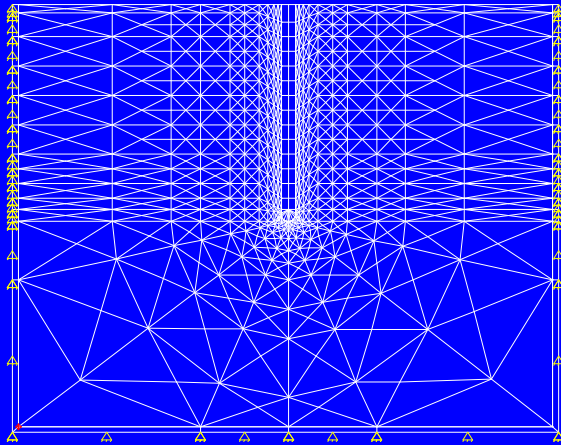


(510 nodes and 934 elements)

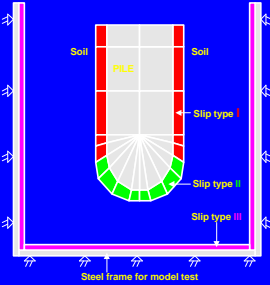


Slip element types,
I and II

Super Mesh-A (slip element types, I, II and III)

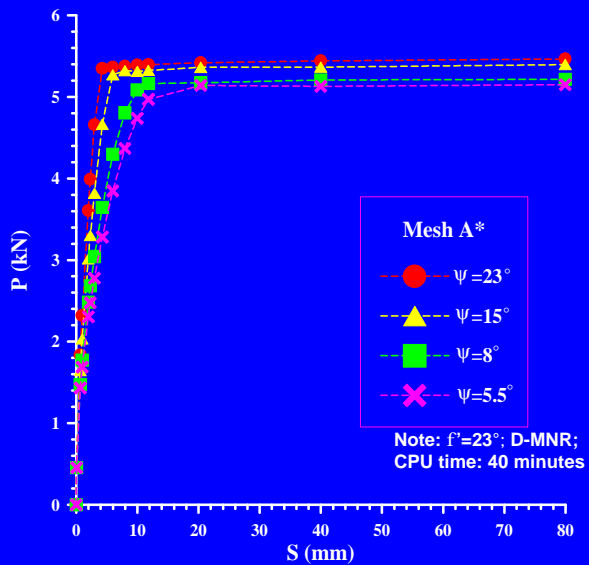


(911 nodes and 1704 elements)

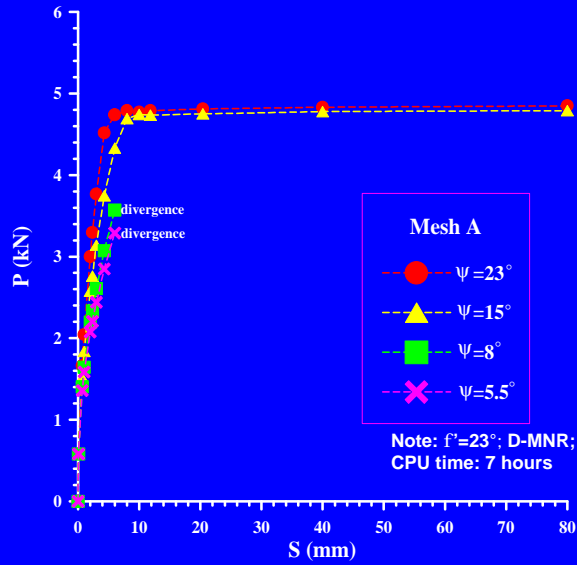


Slip element types,
I, II and III

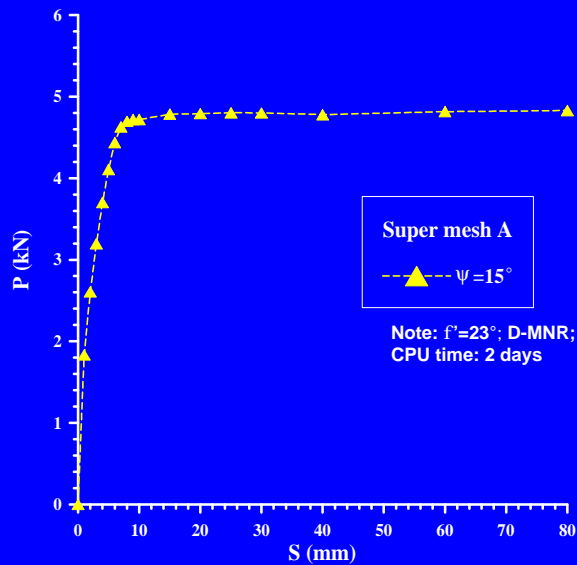
P-S curve for Mesh-A*



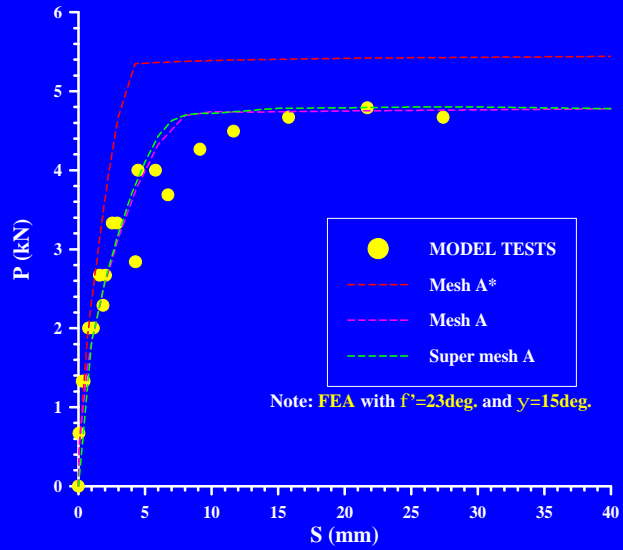
P-S curve for Mesh-A



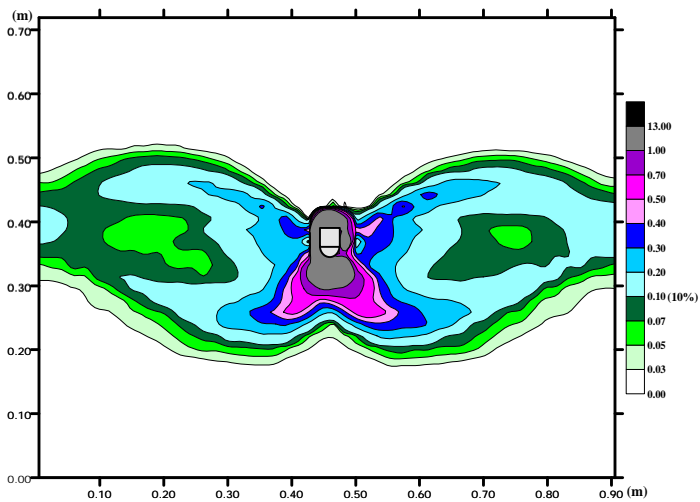
P-S curve for Super mesh-A



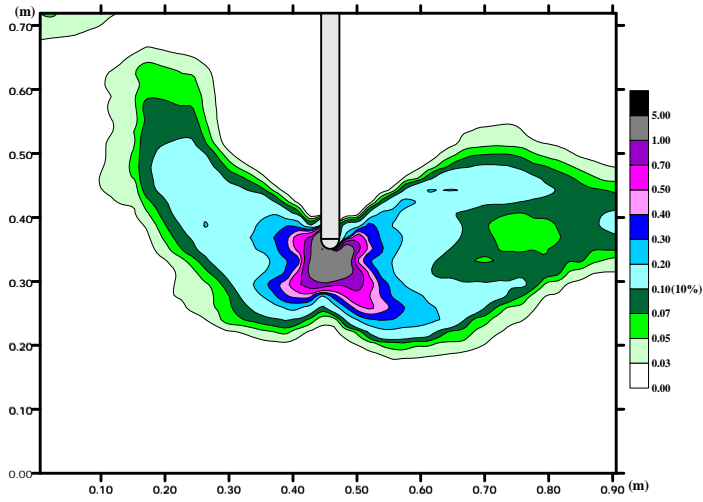
COMPARISON to MODEL TEST data



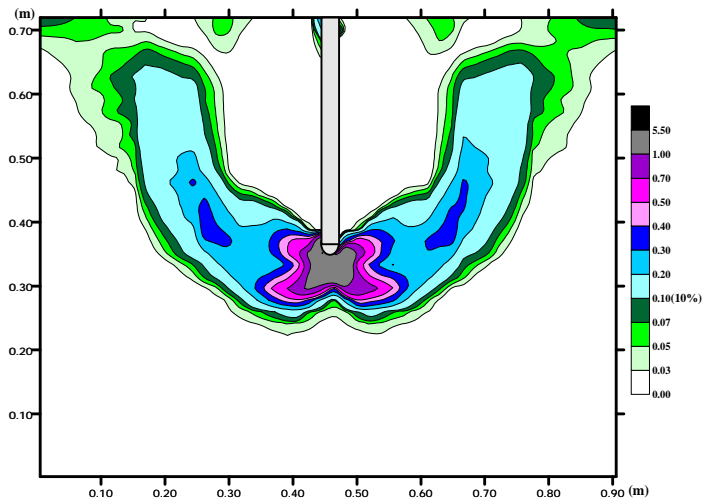
g_{\max} from Mesh A* at S=40mm



g_{\max} from Mesh A at S=40mm



g_{\max} from Super mesh A at S=40mm



Conclusions:

- In order to satisfy the convergence criteria using **slip elements**, difference between ϕ' and ψ was found to be **10 to 13**. However, using **roller boundary** is independent of the degree of non-associate flow.

Slip elements	$f'-y$
No slip elements	23
With slip elements	10 - 13

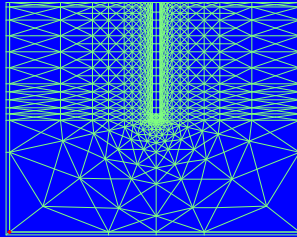
- Maximum shear strain (γ_{\max}) at the large pile displacement is significantly influenced by **the lateral roller boundaries** which commonly used in the conventional FE mesh. However, the author improved this situation by adopting “**slip element type III**” for his real physical model boundary conditions. It is noted that the surface (or/interface) friction angle (d_w) from Casagrande shear box test was applied in the slip element type III.

Suggestions for CRISP:

- Fully implementation of **zero extension line directions** (positive direction is only available at moment) at **one integration point** only;
- Generation of **incremental** vertical and horizontal displacement contours (e.g. plastic region between $S=8\text{mm}$ and $S=40\text{mm}$).

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