

BLOCK ANALYSIS METHOD **AND ITS APPLICATIONS**

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16th CRISP User Group Meeting

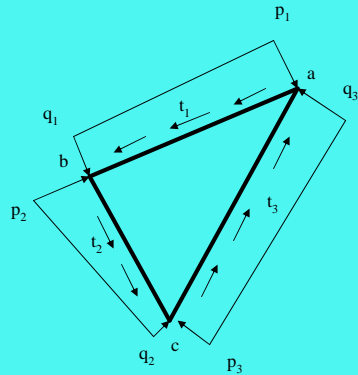
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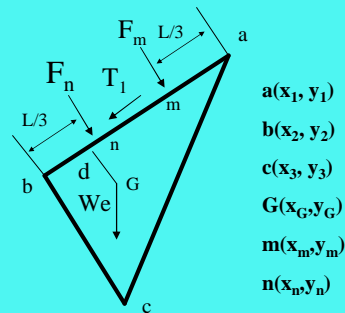
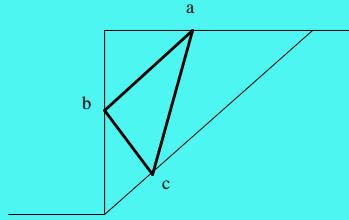
CONTENTS

- Equilibrium equations
- Yield condition
- Linear programming
- Example:
 - Vertical cut (1), Straight line;
 - Vertical cut (2), Search optimum slipping lines
- Conclusion

Block element:



Forces on the element



$a(x_1, y_1)$
 $b(x_2, y_2)$
 $c(x_3, y_3)$
 $G(x_G, y_G)$
 $m(x_m, y_m)$
 $n(x_n, y_n)$

Equilibrium equations:



$$F_m = \frac{1}{2} l p_1 \quad T_1 = t_1 l$$

$$F_n = \frac{1}{2} l q_1 \quad \mathbf{W}_e = \mathbf{S} * \mathbf{g}$$

$$\left. \begin{aligned} F_{mx} &= \frac{1}{2} p_1 (y_1 - y_2) & F_{my} &= \frac{1}{2} p_1 (x_2 - x_1) \\ F_{nx} &= \frac{1}{2} q_1 (y_1 - y_2) & F_{ny} &= \frac{1}{2} q_1 (x_2 - x_1) \\ T_{1x} &= t_1 (x_2 - x_1) & T_{1y} &= t_1 (y_2 - y_1) \end{aligned} \right\}$$

* S is the area of the element; L is the length of the side "ab"; γ is unit weight of soil.

“ab” side on the element:

$$\left. \begin{aligned} S_{1x} &= F_{mx} + F_{nx} + T_{1x} \\ S_{1y} &= F_{my} + F_{ny} + T_{1y} \\ S_{1m} &= F_{mx}(y_G - y_m) + F_{nx}(y_G - y_n) - F_{my}(x_G - x_m) \\ &\quad - F_{ny}(x_G - x_n) + t_1 \cdot l \cdot d \end{aligned} \right\} \begin{bmatrix} S_{1x} \\ S_{1y} \\ S_{1m} \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{bmatrix} \begin{bmatrix} p_1 \\ q_1 \\ t_1 \end{bmatrix}$$

$$a_{11} = a_{12} = \frac{1}{2}(y_1 - y_2), \quad a_{13} = x_2 - x_1$$

$$a_{21} = a_{22} = \frac{1}{2}(x_2 - x_1), \quad a_{23} = y_2 - y_1$$

$$a_{31} = \frac{1}{2}[(y_2 - y_1)(y_G - y_m) + (x_2 - x_1)(x_G - x_m)]$$

$$a_{32} = \frac{1}{2}[(y_2 - y_1)(y_G - y_n) + (x_2 - x_1)(x_G - x_n)]$$

$$a_{33} = -dl$$

For an element:

$$\bullet [S_e] = [A_e][R_e]$$

$$[A_1 \quad A_2 \quad A_3] \begin{bmatrix} R_1 \\ R_2 \\ R_3 \end{bmatrix} + \mathbf{I} \begin{bmatrix} 0 \\ -Sg \\ 0 \end{bmatrix} = 0$$

$$[A_e][R_e] + [W_e]\mathbf{I} = 0$$

For whole structure:

$$[A][R] + [W]\mathbf{I} = 0$$

$$[A] = \begin{bmatrix} A_{e1} & 0 & \dots & \dots & 0 \\ 0 & A_{e2} & \dots & \dots & \dots \\ \dots & \dots & \dots & \dots & \dots \\ \dots & \dots & \dots & \dots & 0 \\ 0 & \dots & \dots & 0 & A_{en} \end{bmatrix}$$

$$[R] = [R_{e1}, R_{e2}, \dots, R_{en}]^T$$

$$[W] = [W_{e1}, W_{e2}, \dots, W_{en}]^T$$

2. Yield condition:

- Tresca material ($\phi = 0$):
- $C_u \geq t_i \geq -C_u, (i=1,2,3)$
 - where C_u is undrained shear strength

3. Linear Programming:

$$\text{Max. } Z = \lambda$$

$$\text{Subject to: } AR+W \lambda = 0$$

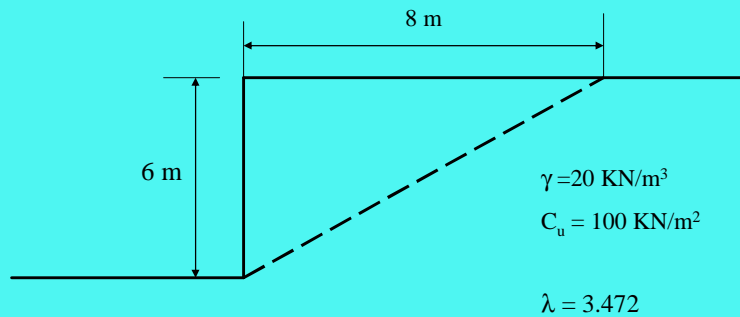
$$C_u \geq t_i \geq -C_u$$

$$\text{all variables } \geq 0$$

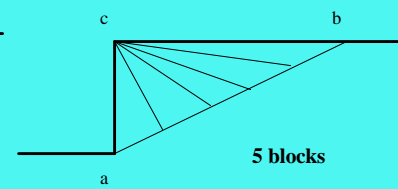
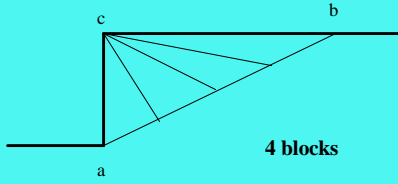
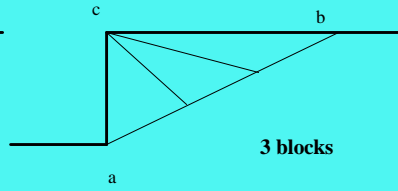
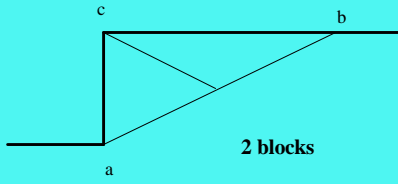


Examples:

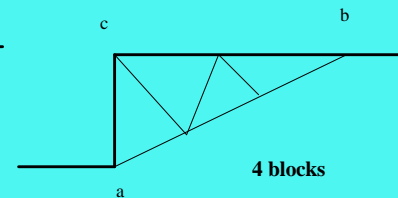
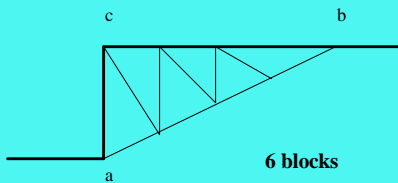
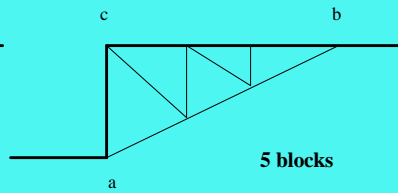
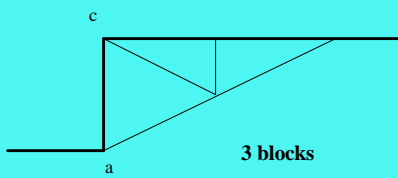
- Vertical cut (1) - straight lines.
 - There are four groups are examined:
 - mother block



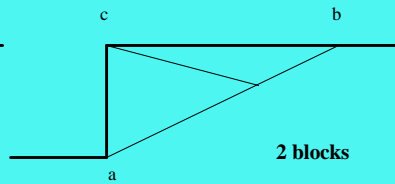
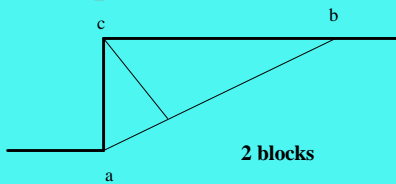
Group 1.



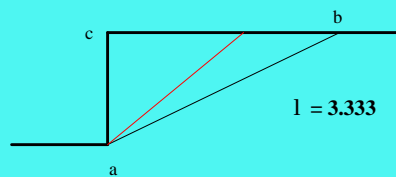
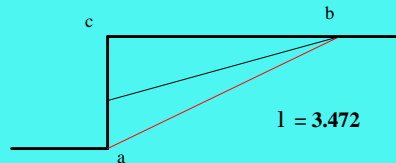
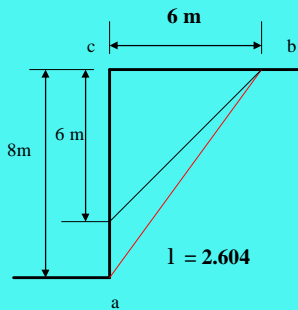
Group 2.



Group 3.



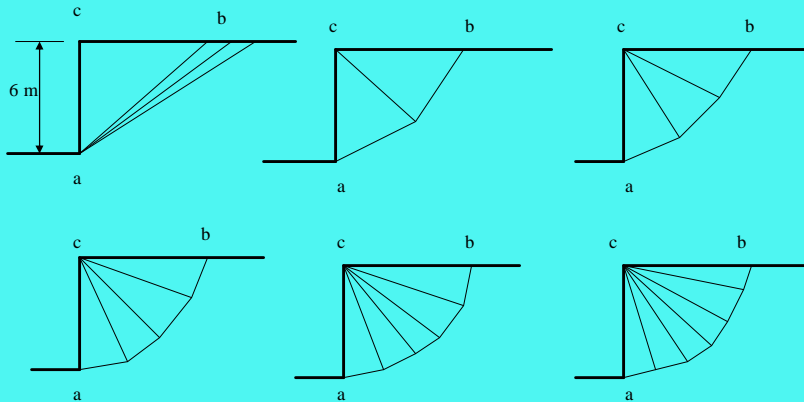
Group 4.



Summary

- 1. Cutting a mother block into smaller son blocks, if all son blocks move together, the load factor is equal to mother block's.
- 2. If son blocks can move separately, the load factor comes from the collapse slipping side.

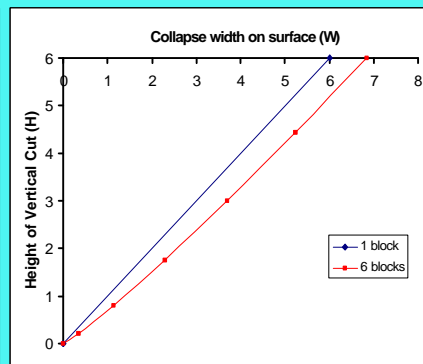
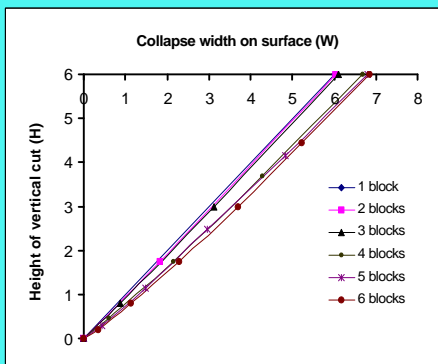
Vertical cut (2): Search optimum slipping lines



Block Analysis Method:

$$h_c = a * \frac{C_u}{g}$$

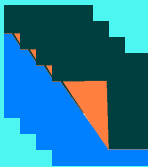
Blocks	1	2	3	4	5	6
α	4	3.946	3.9	3.791	3.767	3.655



Results:

$$h_c = \mathbf{a} * \frac{C_u}{\mathbf{g}}$$

<u>Upper bound:</u>	α	<u>Lower bound:</u>	α
Coulomb	4	Drucker et al (1952)	2
Taylor(1948)	3.83	Heyman (1973)	$2\sqrt{2}$
Chen et al (1969)	3.83	Paster (1978)	3.635
<u>Finite Element method:</u>		<u>Block Analysis method:</u>	
Cascini (1983)	3.764	Authors	3.655



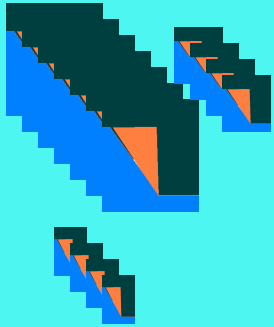
Conclusion

Block Analysis Method can be used in the stability analysis of soil structures.

It has been employed in the stability analysis of vertical cuts and plane strain headings.

It is possible to develop new elements (2D and 3D) and calculate complex stability problems.





Thank you!

